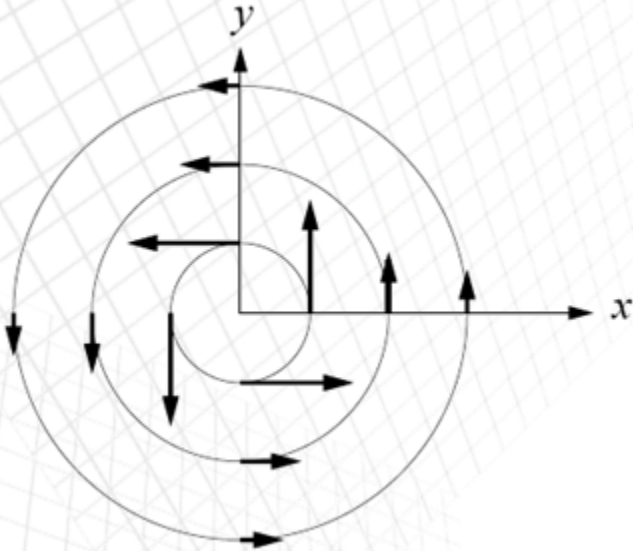


## < 3.14. Vortex Flow >



By definition,

$$V_{\theta} = \frac{\text{const}}{r}, \quad V_r = 0$$

$$\Gamma = \oint \vec{V} \cdot d\vec{s} = -V_{\theta} \cdot (2\pi r)$$

$$\rightarrow V_{\theta} = -\frac{\Gamma}{2\pi r}$$

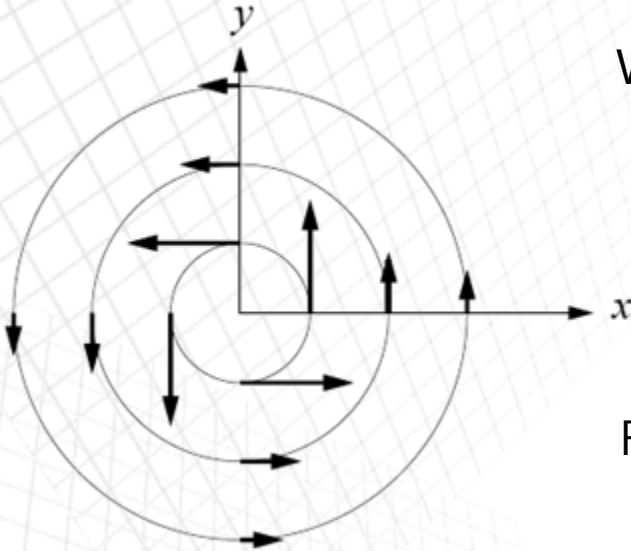
$$\rightarrow \psi = \frac{\Gamma}{2\pi} \ln r$$

$$\rightarrow \phi = -\frac{\Gamma}{2\pi} \theta$$

(NOTE)

1. Vortex flow is irrotational except its origin
2. Circulation is positive-clockwise

## < 3.14. Vortex Flow >



What happens at  $r=0$  ?

$$\Gamma = - \iint_S (\nabla \times \vec{V}) d\vec{S}$$

$$2\pi C = \iint_S (\nabla \times \vec{V}) d\vec{S} \quad \because C = -\frac{\Gamma}{2\pi}$$

For 2D flow

$$2\pi C = \iint_S |\nabla \times \vec{V}| dS$$

$\Gamma$  is the same for all the circulation streamlines

$$\lim_{dS \rightarrow 0} \iint_S |\nabla \times \vec{V}| dS = |\nabla \times \vec{V}| dS \rightarrow 2\pi C = |\nabla \times \vec{V}| dS$$

$$\text{As } r \rightarrow 0 \quad ds \rightarrow 0 \quad \rightarrow \quad \nabla \times \vec{V} \rightarrow \infty$$

## < 3.15. Lifting Flow over a Cylinder >

### ❖ Uniform flow + doublet + vortex

$$\psi = (V_{\infty} r \sin\theta) \left(1 - \frac{R^2}{r^2}\right) + \frac{\Gamma}{2\pi} \ln \frac{r}{R}$$

$$\frac{1}{r} \frac{\partial \psi}{\partial \theta} = V_r = \left(1 - \frac{R^2}{r^2}\right) V_{\infty} \cos\theta$$

$$-\frac{\partial \psi}{\partial r} = V_{\theta} = -\left(1 + \frac{R^2}{r^2}\right) V_{\infty} \sin\theta - \frac{\Gamma}{2\pi r}$$

# Inviscid & Incompressible flow

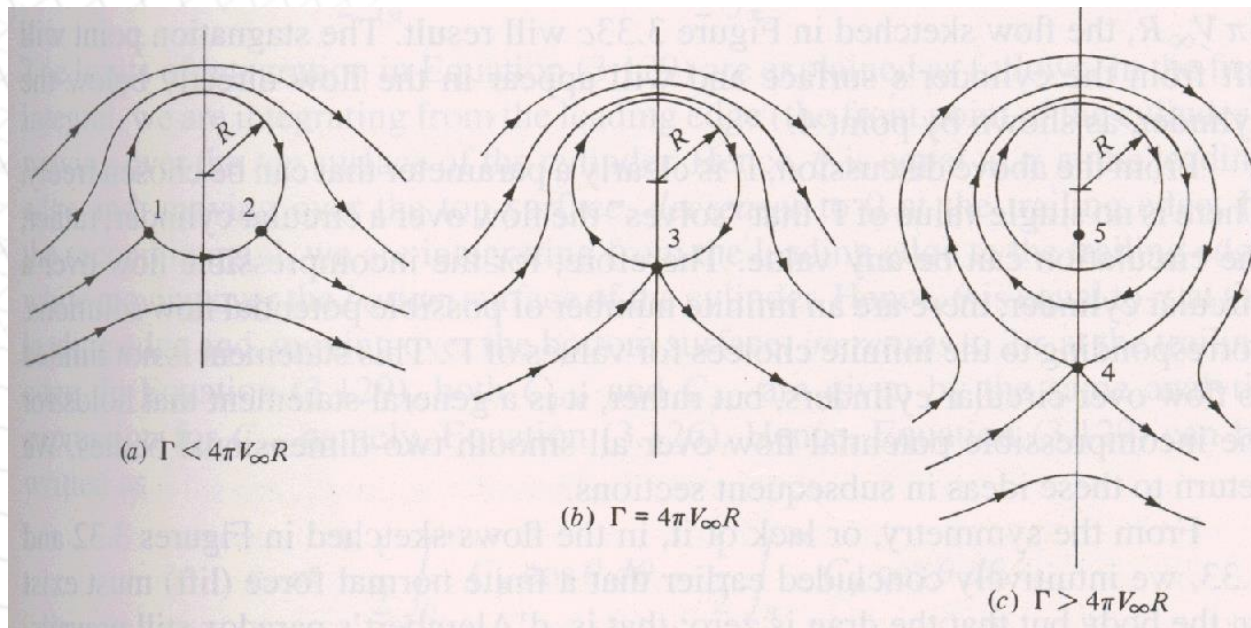
## < 3.15. Lifting Flow over a Cylinder >

### ❖ Stagnation point

$$V_r = V_\theta = 0$$

$$(r, \theta) = \left( R, \sin^{-1} \left( -\frac{\Gamma}{4\pi V_\infty R} \right) \right)$$

Not valid for third case



## < 3.15. Lifting Flow over a Cylinder >

At surface,

$$V_{\theta} = -2V_{\infty} \sin\theta - \frac{\Gamma}{2\pi R}$$

$$\rightarrow C_p = 1 - \left(\frac{V}{V_{\infty}}\right)^2 = 1 - \left(4\sin^2\theta + \frac{2\Gamma\sin\theta}{\pi R V_{\infty}} + \left(\frac{\Gamma}{2\pi R V_{\infty}}\right)^2\right)$$

$$c_d = \frac{1}{c} \int_{LE}^{TE} (C_{p,u} - C_{p,l}) dy \quad \rightarrow \quad c_d = 0$$

→ The drag on a cylinder is zero, regardless of whether or not having circulation in inviscid, irrotational and incompressible flow.



# Inviscid & Incompressible flow

## < 3.15. Lifting Flow over a Cylinder >

Put  $C_p$  expression into this integral

$$c_l = \int_0^c (C_{p,l} - C_{p,u}) dx \quad \rightarrow \quad c_l = \frac{\Gamma}{RV_\infty}$$

Sectional Lift,  $L' = q_\infty S c_l$

$$= \frac{1}{2} \rho V_\infty^2 S c_l = \frac{1}{2} \rho V_\infty^2 S \frac{\Gamma}{RV_\infty}$$

$$= \rho V_\infty \Gamma$$

( $S = 2R$  : planform area)

$$\therefore L' = \rho V_\infty \Gamma$$

"Kutta-Joukowski Theorem"